International Journal of Civil Engineering and Geo-Environment

Journal home_page:http://ijceg.ump.edu.my ISSN:21802742

Engineering Geological Assessment of the Proposed Kakasharaf Dam, Lorestan, Iran

Z. Heidary Nezhad¹, A.H. Haghiabi^{2*}, H.R. Ramazi³

¹ Msc, Spd Engineering Group, Tehran, Iran.

²Associate Professor, Water Engineering Department, Faculty of Agriculture, Lorestan University, Iran.

³ Associate Professor, Mining Department, Amirkabir University of Technology, Tehran, Iran.

ARTICLE INFO

ABSTRACT

Keywords: Dam Permeability Uniaxial Modulus of elasticity Stability This paper describes the results of the engineering geological investigations and rock mechanics studies carried out at the proposed Kakasharaf Dam site. Analyses were carried out in terms of rock mass classifications for diversion tunnel, permeability of the dam foundation and determination of rock mass strength parameters. In this study, the Kakasharaf dam site, constructed on the Kakasharaf River to the south east of Khorramabad in Lorestan province, south western Iran, was investigated from the stand point of the aforementioned engineering geological aspects. The proposed Kakasharaf Dam site is located on sedimentary rock of the upper Cretaceous age and on Quaternary deposits. Sedimentary rocks consist of Buff-grey limestone, marl limestone and shale limestone. Studies were carried out both at the field and the laboratory. Field studies include engineering geological mapping, intensive discontinuity surveying, core drilling, pressurized water tests and sampling for laboratory testing. Uniaxial and tensile strength tests were performed and deformation parameters, unit weight and porosity were determined on the intact rock specimens in the laboratory. Rock mass strength and modulus of elasticity of rock mass are determined using Hoek-Brown empirical strength criterion. Engineering geological investigations, test result and computations indicated that there will be no foundation stability problems. Detailed geotechnical investigations are required for the final design of the dam.

1. Introduction

The proposed Kakasharaf Dam will be built on the Kakasharaf River, 20 km south east of Khorramabad in Lorestan province, south western Iran (Figure 1). It will be used for flow control and water storage for irrigation projects. The Kakasharaf Dam has a crest length of 340m, a maximum high above river bed level of 70 m, and a total storage capacity of 26 million m³.

Geotechnical investigations have been carried out at the project site and in the laboratory. Various laboratory and in-situ tests were performed to assess the characteristics of rock masses. Detailed discontinuity surveying was also carried out.

2. The Geology of the Studied Area

Geological factors play a major role in designing and constructing a dam. Of the various natural factors that influence the design of dams, none are more important than the geological ones. There exist numerous examples of projects where the conditions of the foundation were not sufficiently known and the cost of construction and treatment greatly exceeded the original budget. Information on the regional geology of the area has given by Tamavan Consulting Engineers Company. The proposed Kakasharaf Dam site is located on sedimentary rock of the upper Cretaceous age and on Quaternary deposits. Sedimentary rocks consist of Buff-grey limestone, marl limestone and shale limestone. A generalized topographic map of dam site with location of boreholes and dam axis is shown in Figure 2. Conglomerates are heterogeneous, massive, grey-red, semi-consolidated, consist of boulder and pebbles within sandy-silty-clay matrix, and are slightly to highly weathered. Buff-grey limestones are well bedded, strong, and micritic with 5 cm of slip cleavage marl. Marl and shale limestone are Dark-grey with intercalation of black shale and sandy green shale contain fracture and slips cleavage and eroded. Quaternary deposits are composed of recent alluvial deposit, scree (soft deposits on slopes), and cone of deposition, young terraces, slope washed and debris cobbles gravel.



Figure 1: Location map of the study area



Figure 2: Locations of the boreholes and dam axis of the Kakasharaf Dam site

Characteristics of Discontinuities 3.

In the study area many fissures and fractures with varying orientation developed in response to tectonic. Quantitative description of discontinuities including orientation, spacing, persistence, roughness, aperture and filling were determined at the site by exposure logging in accordance to ISRM (1978). The strikes and dips of 300 joints on the left shore of the dam, and 364 joints on the right shore were measured. Discontinuity orientations were evaluated utilizing a computer program based on equal-area stereo graphic projection namely Dips 5.1 (Diederichs and Hoek, 1989).

The dominant discontinuities sets are distinguished on the left and right shore are shown in Figure 3 and Figure 4. Right shore dominant discontinuity sets;

1m: 67/023 83/43 2m: 47/49 3m: 4m: 35/232

Left shore dominant discontinuity sets;

1m:	19/ 57
2m:	67/026
3m:	80/330





Figure 3: Dominant joint sets on right bank of the Kakasharaf Dam site.



Figure 4: Dominant joint sets on left bank of the Kakasharaf Dam site.

The discontinuities are filled by clay, calcite, limonite, hematite and silica. It is noted that in some section of Kakasharaf Dam site, the clay fillings have been leached by surface waters.

During the field surveys, engineering geological map of the Kakasharaf Dam site and the geological cross section along the dam axis was constructed. In addition, an examination was made of 1759 m of the core, from 25 boreholes drilled by the General Directorate of state hydraulic works. The RQD values of the left shore and right shore were determined. The histograms shown in Figure 5 were prepared using RQD divisions proposed by Deere (1962). From this figure, the rock quantities of the right shore have the following distribution: 4% excellent, 15% good, 16% fair, 21% poor, and 44% very poor. Similarly, the left shore have the following distribution of rock quality: 1% excellent, 6% good, 17% fair, 27% poor, and 49% very poor. Table 1 shows the main orientation, spacing, persistence, aperture and roughness of discontinuities. These were described using the scan-line survey Method following the ISRM (1978) description criteria.



Figure 5: The RQD values of the left shore and right shore.

Properties	Spacing	Description	Percentage	
-			ml	Shl
Spacing (mm)	<20	Extremely close spacing	7	10
	20-60	Very close spacing	29	15
	60-200	Close spacing	35	43
	200-600	Moderate spacing	25	24
	600-2000	Wide spacing	4	8
Persistence(m)	<1	Very low persistence	28	
	1-3	Low persistence	60	
	3-10	Medium persistence	12	
	10-20	High persistence	-	
	>20	Very high persistence	-	
Aperture (mm)	< 0.1	Very tight	10	12
	0.1-25	Tight	8	3
	0.25-50	Partly open	13	16
	0.50-2.5	Open	18	15
	2.5-10	Moderately wide	48	45
	>10	Wide	3	9
Roughness	IV	Rough undulating	10	7
	V	Smooth undulating	5	5
	VI	Slickenside undulating	9	3
	VII	Rough planar	62	76
	VIII	Smooth planar	6	5
	IX	Slickenside planar	8	4

Table 1: Engineering properties of joints and bedding surfaces and their percentage distribution.

4. Permeability Testing

During core drilling, pumping tests were carried out and the permeability of the sedimentary rocks is expressed in terms of Lugeon values. A total of 225 pumping tests were performed at the sedimentary rock units in 22 boreholes. Lugeon values and Test ratio of the sedimentary rocks at Kakasharaf Dam site is shown in Table 2.

Id	Lugeon values	No. of tests	Test ratio	Description
1	>25	83	37	Highly permeable
2	25-5	84	38	Permeable
3	5-1	36	16	Slightly
				permeable
4	<1	20	9	Impermeable

5. Physical and Geomechanical Characteristic of the Marl Limestones

Geomechanical characteristics of a total of 12840 mm core samples of marl limestone were determined in the Engineering Geology Laboratory. The dry unit weights, saturated unit weights, porosity, weighted water absorptions, uniaxial compressive strengths, Poisson ratios, velocities of P and S waves and dynamic and static elasticity modules for the marl limestones were determined on the basis of ASTM (1980, 1996).

Table 3: Statistical evaluation of index and geomechanical properties of marl limestones in the study area.

Properties	Min	Max	Average	Variance	Standard Deviation
/	2 480	2 600	2 5 60	0.004	0.600
Saturated unit weight, $\frac{r}{s}$ ($\frac{t}{m^3}$)	2.400	2.000	2.300	0.004	0.090
Dry unit weight, r/r (t/r)	2.410	2.560	2.510	0.006	0.077
$d^{\prime}/d^{\prime}/m^{3}$					
Water absorption by weight, <i>Aa</i> (%)	0.640	4.570	2.310	0.777	0.881
Porosity, n (%)	1.640	10.850	5.250	0.002	0.0467
Dry Poisson ratio, V_n	0.120	0.300	0.210	0.002	224.970
P ware velocity, v_p (m/s)	0.120	0.310	0.240	50612.600	224.970
S ware velocity, v_s (m/s)	5173	6084	5545.460	9030.140	95.020
Point load strength index, is 50 (MPa)	2870	3188	30340330	0.302	0.549
Uniaxial compressive strength, (MPa)	3.030	4.360	68.410	19.770	24.896
Static elasticity modules, E_s (GPa)	35.780	47.010	47.520	24.011	0.881
Dynamic elasticity modules, E _d (GPa)	59.740	70.470	65.920	18.188	4.264

6. Physical and Geomechanical Characteristics of the Shale Lime Stones

Geomechanical characteristics of a total of 15810 mm core samples of shale limestone were determined in Engineering Geology Laboratory.

The dry unit weights, saturated unit weights, porosity, weighted water absorptions, uniaxial compressive strengths, Poisson ratios, velocities of P and S waves and dynamic and static elasticity modules for the shale limestones were determined on the basis of ASTM (1980, 1996) And ISRM (1978). Minimum, maximum, average

and standard deviation for these parameters are given in Table 4.

7. Engineering Classification of the Rock Mass

The marl limestones and shale limestones were classified according to the RMR (Bieniawski, 1989) system in order to determine what kinds of support systems should be used in the diversion and power tunnels. RMR values, the parameters used in rock- mass classification and corresponding point totals for best- and worst- case-scenarios, are given in Table 5 and Table 6 and Table 7.

Properties	Min	Max	Average	Variance	Standard Deviation
			-		
Saturated unit weight, $\frac{r}{s}$ ($\frac{t}{m^3}$)	2.500	2.680	2.620	0.001	0.040
Dry unit weight, r/d (t/m^3)	2.440	2.690	2.590	0.003	0.050
Water absorption by weight, A_a (%)	0.640	2.750	2.250	0.360	0.600
Porosity, n (%)	1.640	6.960	3.190	2.160	1.470
Dry Poisson ratio, V_n	0.450	0.220	0.180	0.0003	0.020
P ware velocity, $v_p(m/s)$	0.160	0.270	0.200	0.0017	0.040
S ware velocity, v_s (m/s)	0.130	5568	5201	52007	228
Point load strength index, is 50 (MPa)	4932	2919	2686	31982	179
Uniaxial compressive strength, (MPa)	2301	4.800	3.470	0.794	0.891
Static elasticity modules, E _s (GPa)	36.080	69.560	55.930	146.130	12.090
Dynamic elasticity modules, Ed (GPa)	30.950	48.170	39.900	39.580	6.290

Table 4: Statistical evaluation of index and geomechanical properties of the shale limestone in the study area



Parameters	Pa	rameters ratir	ng or description	
Uniaxial compressive strength, (MPa)	Min	Rating	Max	Rating
Rock Quality Designation (%)	4	1	120	12
Spacing of discontinuities (m)	10	3	95	20
Condition of discontinuities continuity (m)	< 0/006	5	> 2	20
Spacing (mm)	> 20	0	< 1	6
Roughness	> 5	0	None	6
Filling	Polished	0	Smooth	1
Weathering degree	None	6	Hard	2
Ground water conditions	Highly	0	Slightly	5
Orientation of discontinuities RMR	Wet	7	Dripping	4
	Unfavorable	-10	Unfavorable	-10
RMR		12		66

Table 6: Classification of the shale limestone at the dam site based on RMR system

Parameters	P	arameters rating	g or description	
Uniaxial compressive strength, (MPa)	Min	Rating	Max	Rating
Rock Quality Designation (%)	2	1	95	7
Spacing of discontinuities (m)	7	3	80	15
Condition of discontinuities continuity (m)	< 0/006	5	> 2	20
Spacing (mm)	> 20	0	< 1	6
Roughness	> 5	0	None	6
Filling	Polished	0	Smooth	1
Weathering degree	None	6	Hard	2
Ground water conditions	Highly	0	Slightly	5
Orientation of discontinuities RMR	Wet	7	Dripping	4
	Unfavorable	-10	Unfavorable	-10
RMR		13		56

Table	Table 7: Classification of marl and shale limestone based on RMR values						
	Marl limestone Shale limestone						
	Worst condition	Best condition	Worst condition	Best condition			
RMR value	12	66	13	56			
Group	V	II	V	III			
Description	Very weak rock	Good Rock	Very weak Rock	Medium Rock			

8. Discussion

Kakasharaf Dam will be built on sedimentary rocks which consist of marl limestone and shale limestone. Quantitative description of discontinuities was performed at the site by exposure logging in accordance with ISRM (1978).

Sedimentary rocks at the site are "slightly permeable "according to pumping test results and grouting is offered to prevent leakage under the dam foundation from permeable zones. On the other hand alluvium was determined as "highly permeable" and was decided to remove it by using the cut-off method. Laboratory tests on core samples were carried out to find the physical parameters. As a result of uniaxial compression tests, marl and shale limestone are in the high strength rock group. Evaluation of marl and shale limestone for rock mass classifications due to RMR values, indicated that marl limestone is in very poor to good quality and shale limestone is in very poor to fair quality.

Strength of rock masses at Kakasharaf Dam site was expressed by using Hock-Brown empirical failure criteria (Hoek et al, 1995). Uniaxial compression strength of the rock for marl and shale limestone is 68 to 41 and 55.93 MPa, respectively. All these results have led to conclusion that foundation rocks are suitable.

9. Conclusion

Kakasharaf Dam, will be located on the sedimentary rocks. Engineering geological investigations, test results and computations indicate that Kakasharaf Dam can be safely constructed on the proposed site.

Acknowledgements

The authors would like to thank ferrydon Bahrami Samani (MSC) and Masood Shrooye (MSC) for their useful suggestions.

References

- ASTM, 1980. Annual Book of ASTM Standards — Natural Building Stones; Soil and Rock. Part 19. ASTM Publication. 634 pp.
- ASTM, 1996. Standard Test Method for Laboratory Determination of Pulse

Velocities and Ultrasonic Elastic Constants of Rock, D2845.

- Bieniawski, Z.T., 1989. Engineering Rock Mass Classifications. Wiley, New York, 251 pp.
- Deere, D. U. 1962. Technical Description of Rock Cores for Engineering Purposes. *Rock Mechanics and Engineering Geology*, 1, 1– 18.
- Diederichs, M. S., Hoek, E. 1989. DIPS 2.2. Advanced Version Computer Program, Rock Engineering Group, Department of Civil Engineering, University of Toronto.
- Hoek, E., Kaiser, P.K., Bawden, W.F., 1995. Support of Underground Excavations in Hard Rock. Balkema, Roterdam, Brookfield, 213 pp.
- ISRM. 1978. Suggested Methods for the Quantitative Description of Discontinuities in Rock Masses. Rock Characterization, Testing and Monitoring. London, Pergamon, Oxford, 221 pp.